HYDROLOGY AND GEOCHEMISTRY OF A SLAG-AFFECTED AQUIFER AND CHEMICAL CHARACTERISTICS OF SLAG-AFFECTED GROUND WATER, NORTHWESTERN INDIANA AND NORTHEASTERN ILLINOIS



U.S. GEOLOGICAL SURVEY Water-Resources Investigations Report 97-4198

Prepared in cooperation with the INDIANA DEPARTMENT OF ENVIRONMENTAL MANAGEMENT, OFFICE OF SOLID AND HAZARDOUS WASTE

U.S Department of the Interior

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Hydrology and Geochemistry of a Slag-Affected Aquifer and Chemical Characteristics of Slag-Affected Ground Water, Northwestern Indiana and Northeastern Illinois

By E. RANDALL BAYLESS, THEODORE K. GREEMAN, and COLIN C. HARVEY

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CONVERSION FACTORS, VERTICAL DATUM, AND ABBREVIATIONS

Temperature in degrees Celsius (°C) can be converted to degrees Fahrenheit (°F) as follows:

 $^{\circ}F=1.8x \ ^{\circ}C+32$

Sea Level: In this report, "sea level" refers to the National Geodetic Vertical Datum of 1929—a geodetic datum derived from a general adjustment of the first-order level nets of both the United States and Canada, formerly called "Sea Level Datum of 1929."

Abbreviations for water-quality units used in this report: Chemical concentrations and water temperature are given in metric units. Volumes of sample are given in liters (L) and milliliters (mL). Chemical concentrations are

Hydrology and Geochemistry of a Slag-Affected Aquifer and Chemical Characteristics of Slag-Affected Ground Water, Northwestern Indiana and Northeastern Illinois

By E. Randall Bayless¹, Theodore K. Greeman¹, and Colin C. Harvey²

Abstract

Slag is a by-product of steel manufacturing and a ubiquitous fill material in northwestern Indiana. Ground water associated with slag deposits generally is characterized by high pH and elevated concentrations of many inorganic water-quality constituents. The U.S. Geological Survey, in cooperation with the Indiana Department of Environmental Management, conducted a study in northwestern Indiana from June 1995 to September 1996 to improve understanding of the effects of slag deposits on the water quality of a glacial-outwash aquifer.

The Bairstow Landfill, a slag- eril mdepos

2 Hydrology and Geochemistry of Slag-Affected Aquifer

The physical properties of slag vary. Such properties as degree of crystallization, vesicularity, density, and particle size are determined largely by the method used to cool the molten material (Lankford and others, 1985). Slag is removed from the furnaces at about 1,480°C and may be cooled slowly in the open air, moderately fast with controlled sprays of water, or quickly by water immersion. Slag densities range from 50 to 156 lb/ft³, depending on the vesicularity (Lankford and others, 1985).

Steel and slag production along the Chicago River began in the late 1830's. In the 1880's, the steel industry moved near the Calumet River in south Chicago. Slag was hauled to Indiana and used as lakeshore protection from erosion wherever the railroads followed the Lake Michigan beach. In 1903, a cement plant was built near Gary Station (later to become Gary, Ind.) to use the slag generated by the south Chicago steel industry for the manufacture of portland cement (Rooney and Carr, 1975, p. 25). In 1906, the steel industry expanded into Indiana, and slag production quickly outpaced the demands of cement manufacturers. During 1945 to 1950, the Gary, Ind., blast furnaces produced 1,000,000 tons of slag annually (Hurley, 1995, p. 20). Slag disposal in swampy, low-lying land at the southern end of Lake Michigan became commonplace to accommodate the oversupply.

In northern Lake County, Ind., more than 20 mi² of the Calumet aquifer is covered with slag and a smaller area is covered by "fill" (Kay and others, 1996b, pl. 2). Slag also is mixed with ash, construction debris, dredging spoils, industrial wastes, municipal wastes, sand, and sludges to create "fill." The thickness of most slag and fill deposits in northwestern Indiana is less than

calcite (CaCO₃) and dolomite (CaMg(CO₃)₂); supersaturated with respect to aluminosilicate minerals, goethite (a-FeO OH), hematite (Fe₂O₃), and magnesite (MgCO₃); undersaturated with respect to amorphous ferric hydroxide (FeOH₃) and iron-sulfide minerals; and nearly saturated with siderite.

Water from wells with pH values greater than 11.0 had elevated concentrations of aluminum and depleted concentrations of magnesium, iron, manganese, and silica relative to the background samples (Roadcap and Kelly, 1994). Calculations using EQ3 indicated that the high pH ground water was undersaturated with respect to feldspars, gibb-site (Al(OH)₃), and kaolinite (Al₄(Si₄O₁₀)(OH)₈). Precipitation of brucite (Mg(OH)₂), high-magnesian calcite (Ca,Mg(CO₃)), iron and manganese carbonate, and oxyhydroxide minerals was thought to explain the relatively low concentrations of magnesium, iron, and manganese in ground water.

Calcium concentrations also were elevated in water from wells with pH values greater than 11.0, relative to background wells (Roadcap and Kelly, 1994). The minerals anorthite $(CaAl_2Si_2O_8)$, dicalcium silicate (Ca_2SiO_4) , melilite ((Ca,Na)₂[(Mg,Fe⁺²,AlSi)₃O₇]), merwinite ($Ca_3Mg(Si_2O_8)$), monticellite ($CaMg(SiO_4)$), rankinite (Ca₃(SiO₇)), spinel (MgAl₂O_{Δ}), and wollastonite (Ca(SiO₃))—all thought to be constituents of slag (Lee, 1974; Loomba and Pandey, 1993)-were below saturation in all samples. Ground water was supersaturated with respect to barite (BaSO₄), chromite (Fe⁺²Cr₂O₄), eskolaite (Cr₂O₃), ilmenite (FeTiO₃), rhodochrosite (MnO₃), rutile (TiO₂), strontianite (SrCO₃), and witherite (BaCO₃).

Purpose and Scope

The purpose of this report is to describe the results of a site investigation examining geochemical processes in a glacial aquifer that is receiving drainage from an overlying slag deposit. Groundwater-quality data from this and a previous study of northwestern Indiana and northeastern Illinois also were used in a statistical evaluation of regional data to evaluate whether slag-affected water can be distinguished from background water.

The Bairstow H. Company site (Bairstow Landfill), in Hammond, Ind., was instrumented with 10 observation wells and samples were collected for mineralogic, geochemical, and water-quality analyses. Geochemical models were constructed on the basis of data from the Bairstow Landfill to examine the potential processes responsible for water-quality changes where slag drainage enters a glacial aquifer. The generalized results of the site-specific investigation are expected to apply to numerous settings throughout the region where variable thicknesses of slag overlay glacial outwash and other sand aquifers.

A total of 137 ground-water-quality analyses from this study and a previous investigation of the Calumet aquifer in northwestern Indiana and northeastern Illinois were statistically summarized. The summary was intended to characterize the range and the variability in ground-water quality in northwestern Indiana and to examine distinguishing characteristics of water from wells screened in

DESCRIPTION OF THE STUDY AREA

The study area is in the Calumet Lacustrine Plain physiographic unit (Schneider, 1966, p. 50). The area was scoured smooth by glacial ice from the Lake Michigan lobe during the Pleistocene epoch. Reoccurring several times over the last million years, glacial ice followed a preferred -

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Methods of Investigation 7

The Bairstow Landfill was selected for sitespecific study because (1) well drillers' records for an on-site observation well indicated that the stratigraphy was typical of northwestern Indiana; (2) analytical data for the on-site observation well indicated that water quality was being affected by slag drainage; (3) the hydraulic gradient in the landfill area was known from the USGS records for the northwestern Indiana data network; (4) surface material and material at depth on exposed slopes appeared to be common blast-furnace slag; and (5) active mineral deposition was occurring along the southern shoreline of Lake George, apparently where ground water was discharging from the landfill. The Bairstow Landfill was selected to represent slag-aquifer systems that are common throughout northwestern Indiana; however, the variability of slag-fill chemistry may make the results of this study less applicable to other locations in northwestern Indiana.

Well Installation

A south-to-north flowline was selected for instrumentation and sampling at Bairstow Landfill along the ground-water-flow direction interpreted from water levels of wells in the USGS network (see line A-A' on fig. 3). The flowline began at the existing well BH-31, ended at Lake George, and was approximately perpendicular to the southern shoreline of Lake George.

The observation-well transect included 10 wells at four sites (figs. 3 and 4). Observation well BH-31 was installed during a previous investigation near the highest accessible elevation at the landfill. The 15-ft screened interval crosses the slag–aquifer interface. Nested observation wells were installed July 16 and 17, 1996, at sites BH-32 and BH-33 at about 510 and 800 ft north of BH-31, respectively. Wells at BH-32 are screened in slag (BH-32SL), in the aquifer just beneath the slag (BH-32S), in the middle of the aquifer (BH-32I), and at the base of the aquifer (BH-32D). Observation wells at BH-33 are installed in the slag (BH-33SL), across the slag–aquifer interface (BH-33S), and in the middle of the aquifer (BH-33I). The naming convention for these wells used "SL," "S," "I," and "D" to indicate "slag," "shallow," "intermediate," and "deep," respectively. The S, I, and D wells also are collectively referred to as "aquifer wells" throughout the report.

Wells at BH-32 and BH-33 were installed using the hollow-stem auger method. Wells at BH-32 and BH-33 were constructed from 2-in.-inner-diameter polyvinyl chloride (PVC) flush-joint casing and 5-ft-long PVC screens with 0.010-slot size. Wells were installed with a 6.75-in. hollow-stem auger. The annular space was backfilled with sand to 2 ft above the screen, bentonite to within 3 ft of land surface, and concrete to the surface.

Two observation wells were installed in the lakebed immediately north of the southern shore of Lake George on July 12, 1996. BH-34SS and BH-34ND are 1,200 ft north of BH-31 and about 5 and 20 ft north of the mean water line, respectively. BH-34SS is screened 2 to 3 ft below the lakebed and at least partially in slag, and BH-34ND is screened about 4.5 to 6.5 ft below the lakebed. Wells BH-34SS and BH-34ND were hand driven with a 36-kg post driver and constructed from 2-in.-diameter stainless-steel pipe with 1-ft stainless-steel screens having 0.010-sized slots. Lakebed wells are designated "ND" and "SS" to indicate "north-deep" and "south-shallow," respectively.

Water-Sample Collection and Analysis

Ground-water samples were collected August 13 through 15, 1996, from the 10 Bairstow Landfill observation wells. An additional sample was collected from Lake George, 2 ft below water surface, near well BH-34ND. Two additional samples were collected from well BH-32S to examine the reproducibility of sampling methodology and analytical precision.



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58 <u>8</u> 582	
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Samples for water-quality analysis were collected by use of a peristaltic pump equipped with Tygon tubing. Sampling preparation included removal of three times the standing volume of water in the well; on-site measurements of pH, specific conductance, redox potential, water temperature, and dissolved oxygen were monitored with a multiparameter probe and a stainless-steel flow-through chamber. On-site measurements were recorded and samples collected after on-site measurements had stabilized. Samples were preserved according to the guidelines specified by the USGS National Water-Quality Laboratory and are described in table 1. Measurements of redox potential are reported as a field measurement relative to the calomel electrode. All samples were analyzed by the USGS National Water-Quality Laboratory for concentrations of inorganic compounds similar to those examined by Duwelius and others (1996); the analytical methods are described in Wershaw and others (1987) and Fishman and Friedman (1989). An incremental titration to determine carbonate alkalinity was done at the site.

Decontamination of the pump, hoses, and flow-through chamber was done between each sampling. Decontamination consisted of pumping an Alconox-water mixture through the flowthrough chamber, pump, and hoses, followed by tap water and deionized water. The pump and hose exteriors were rinsed between wells with deionized water.

Solid-Phase Sampling and Analysis

Solid-phase samples were collected during installation of all wells, except BH-31. Handdriven split-spoon samples were collected in liners at BH-34 sites and immediately sealed with beeswax. Split-spoon sampling was not capable of capturing slag or sand at sites BH-32 and BH-33. Samples at sites BH-32 and BH-33 were taken from auger cuttings and from the auger bit as it was retracted from the screened interval. Auger cuttings and bit samples were preserved in zip-lock freezer bags and refrigerated until solid-phase analysis in August and September 1996. The geochemistry and mineralogy of solid samples were determined at the Indiana University Department of Geological Sciences. Analyses included (1) a determination of solid chemistry from sample digestion and major and minor element quantification using neutron activation or ion chromatography and plasma spectroscopy, and (2) a description of bulk mineralogy based on X-ray diffraction.

Sixteen solid-phase samples were analyzed for geochemistry and mineralogy. The sample distribution included two slag samples, one sample from the slag–sand interface, three sand samples below the sand–slag interface, one sample of the Lake Border lacustrine deposit subdivided into three grain-size fractions ($<2 \mu m$, 2–5 μ **Table 1.** Sample-preservation requirements for ground-water samples collected at Bairstow Landfill, Hammond, Ind.,

 August 1996

 $[ml, milliliter; \mu m, micrometer; ^{\circ}C, degrees \ centigrade; <, less \ than; HNO_3, nitric \ acid]$

Analytes	Sample container, preparation, and preservation
Nitrite plus nitrate, as nitrogen; nitrite, as nitrogen; ammonia, as nitrogen; ammonia plus organic nitrogen, as nitrogen; phosphorous; and orthophos- phate, as phosphorous	One 125-ml brown polyethylene bottle, field rinsed, filtered with a 0.45-µm filter, and maintained at 4°C
Potassium, iron, magnesium, manganese, calcium, silica, and sodium	One 250-ml polyethylene bottle, acid rinsed, filtered with a 0.45- μ m filter, acidified with HNO ₃ to pH<2 and maintained at 4°C
Residue on evaporation at 180°C and lab alkalinity	One 250-ml polyethylene bottle, field rinsed, unfiltered, nonacidified, and maintained at 4°C
Chloride, sulfate, and fluoride	One 500-ml polyethylene bottle, filtered with a 0.45-µm filter, nonacidified, and maintained at 4°C
Arsenic, aluminum, antimony, barium, beryllium, cadmium, chromium, cobalt, copper, lead, manga- nese, molybdenum, nickel, selenium, silver, uranium, zinc	One 250-ml polyethylene bottle, acid rinsed, filtered with a 0.45- μ m filter, acidified with HNO ₃ to pH<2, and maintained at 4°C
Lab pH and lab specific conductance	One 250-ml polyethylene bottle, field rinsed, nonacidified, nonfiltered, and maintained at 4°C



The $<\!\!45\text{-}\mu\text{m}$ samples from the Lake Border lacustrine sediment were further separated into $<\!\!2\text{-}$

indices do not indicate whether an undersaturated mineral that is not present in the solid phase has been removed by dissolution or whether it was never present.

Mass-Balance Calculations

The computer program NETPATH (Plummer and others, 1994) was used to generate massbalance models along a ground-water flowpath at Bairstow Landfill. The mass-balance models were used to indicate the relative proportions of precipitating and dissolving minerals that could account for the observed differences in water quality between wells in the Bairstow Landfill.

NETPATH generates models based on minerals specified by the user to be important in the geochemical system. The specified minerals are added to or removed from the ground-water system in the computation to account for the differences in the concentrations of water-quality constituents between two wells. In addition to mineral precipitation and dissolution, NETPATH can calculate proportions of mixed ground-water components that can combine with the mineral precipitation and dissolution to account for changes in constituent concentrations. The number of models generated by NETPATH is based on the number of waterquality constituents, solid phases, and other processes selected by the user to potentially explain the changes in water quality.

Statistical-Summary Calculations

Data from this study (8 sites) and from Duwelius and others (1996; 129 wells sampled in June 1993) were used to characterize the range and variability of constituent concentrations in slag-affected ground water of northwestern Indiana and northeastern Illinois. Ground-water samples collected for both studies were analyzed for the same water-quality constituents and properties. The statistical summary was intended to identify water-quality constituents and properties that may be indicators to distinguish water from slag-contact wells, slag-affected wells, or background wells. A geographical information system (GIS) was used to superimpose locations of the 137 ground-water-sample sites on digital maps describing (1) locations of known fill deposits (Kay and others, 1996b), (2) ground-water levels (Duwelius and others, 1996), (3) well depths, (4) stratigraphy, and (5) fill thicknesses (Kay and others, 1996a). Results of this study identified 3 subsets of wells that may represent common settings in northwestern Indiana, including 21 slag-contact wells, 25 slag-affected wells, and 11 background wells. Eighty observation wells were removed from the data set because water quality at those sites could

Hydrology

A potentiometric-surface map (Greeman, 1995) was constructed from quarterly measurements of water levels in a regional network of 76 monitoring wells. That map indicates regional ground-water flow in the Calumet aquifer near the site is generally toward Lake Michigan (Greeman, 1995); ground-water flow near the Bairstow Landfill is usually toward Lake George (fig. 3).

The ground-water flowpaths, based on water levels in the Bairstow wells, indicate that recharge moves down through the slag pile and uppermost sands into the intermediate-depth sands. Ground water also moves up from the deeper sands to converge at the intermediate-depth sands, where ground water gains a strong horizontal component of flow toward Lake George. Ecology and Environment, Inc., (1993) noted an unidentified white leachate material entering Lake George from the northwestern corner of the Bairstow Landfill, suggesting ground-water discharges to Lake George.

Ground-water flow at the site is affected by Lake George, the wetlands bordering the east side of the site, and by induced drawdown on the property of the Amoco petroleum-tank farm. Drawdown of the water table is induced at the Amoco site to inhibit off-site migration of nonaqueous-phase liquids (fig. 3). The possibility exists for ground-water-flow direction at the study site occasionally to be reversed to north-to-south in response to local drawdowns produced by the Amoco barrier wells or elevated water levels in Lake George; as a result of the data collected by this study, however, conclusions cannot be made about occurrences of flow reversals.

Ground-Water and Surface-Water Chemistry

At the Bairstow Landfill, alkalinity, dissolved solids, pH, and specific conductance varied similarly with respect to depth or stratigraphic position and were distinctly highest in the water from the slag wells (BH-31, BH-32SL, BH-33SL, and BH-34SS) (fig. 6; table 2, back of report). Alkalinity values ranged from 626 to 903 mg/L as $CaCO_3$ in the water from the slag wells and 420 to 590 mg/L as $CaCO_3$ in all other wells. Alkalin-

Ground-Water and Surface-Water Chemistry 17

As with the general water-quality properties, the distribution of the major ions and silica at Bairstow Landfill showed distinct patterns related chiefly to depth or stratigraphic position (fig. 7). Major ions (including calcium, magnesium, potassium, sodium, bicarbonate alkalinity, chloride, fluoride, sulfate, and ammonium) generally compose most of the dissolved mass in these water samples. Concentrations of calcium, potassium, and sulfate were highest in wells screened (at least partly) in slag; silica was highest in wells screened below the slag–aquifer interface; and magnesium was highest in intermediate and deep wells. The relative abundances of the carbonate species $H_2CO_3-HCO_3^{-}-CO_3^{2-}$ are pH dependent, with H_2



Nickel concentrations in water ranged from 9 to 13 μ g/L in slag wells and from 2 to 6 μ g/L in all other wells. Selenium concentrations in water ranged from 2 to 4 μ g/L in slag wells and were below reporting limits (<1 μ g/L) in all other wells.

The trace elements chromium, lead, and zinc generally were more abundant in water from wells positioned immediately below the slag-aquifer interface. Chromium concentrations were less than the laboratory reporting limits in water from the four slag wells, the sample from Lake George, and BH-32D. By comparison, chromium concentrations ranged from 2 to 4 μ g/L in water from wells BH-32S, BH-32I, BH-33S, and BH33I. Lead concentrations were 6, 15, 12, and $2 \mu g/L$ in water from wells BH-32S, BH-33S, BH-33I, and in the sample from Lake George, respectively, but were less than the laboratory reporting limit in all other wells. The lead concentration in the sample from BH-33S, 15 μ g/L, was equal to the USEPA maximum contaminant level for lead (U.S. Environmental Protection Agency, 1992). Zinc concentrations ranged from 2 to $3 \mu g/L$ in the four slag wells, BH-32I, BH-32D, and the sample from Lake George but were greater in water from wells BH-32S, BH-33S, and BH-33I, respectively.

Iron and manganese were most abundant in water from deeper aquifer wells, and conranged from 13.0 to 20.0 mg/L in BH32S, BH-33S, and BH-33I and ranged 2.60 to 3.90 mg/L in all other wells and 0.90 mg/L in the sample from Lake George. Orthophosphate concentrations ranged from 0.11 to 0.47 mg/L in the shallow and intermediate-depth aquifer wells at BH-32 and BH-33; concentrations ranged from <0.01 to 0.07 mg/L in all other samples. The highest orthophosphorous concentration (0.57 mg/L) was measured in well BH-32S. Total phosphorous ranged from 0.39 to 0.63 mg/L in wells BH-32S, BH-33S, and BH-33I and ranged <0.01 to 0.08 mg/L in all other wells.

Solid-Phase Geochemistry

Concentrations of cadmium, calcium, chromium, copper, iron, lead, manganese, niobium, phosphorus, tungsten, vanadium, and zinc concentrations generally were greater in slag samples than in samples of the Calumet aquifer sand and the Lake Border sequence lacustrine sediment. Slag samples were depleted in aluminum, potassium, scandium, and sodium relative to samples of the Calumet aquifer sand and the Lake Border sequence lacustrine sediment. By comparison, analyses of samples from 1 to 2 ft below the bases of three slag piles at Bairstow Landfill found concentrations of barium, calcium, chromium, copper, iron, manganese, nickel, selenium, and vanadium that were elevated relative to a background sample collected from a park about 1.2 mi north of the Bairstow Landfill (Roy F. Weston, Inc., 1995). In the 1995 Weston sample, collected from the slag pile nearest the study transect, the elements aluminum, beryllium, potassium, cobalt, silver, and arsenic also were detected.

The elements barium, copper, lead, nickel, sodium, strontium, titanium, vanadium, and zinc commonly occurred in concentrations ranging from 0.1 to 1.0 percent of the total mass of most samples. Concentrations in the range 0.1 to 1.0 percent were sometimes large enough to cause mineral precipitation and ion substitution that were apparent in X-ray diffractograms; minrecordite (CaZn[CO₃]₂) is an example. Two noticeably high lead, strontium, and zinc concentrations are associated with lakebed samples 34A and 34C (and possibly sample 34B). Copper concentrations were elevated in all lakebed sediments. Copper and lead concentrations at the site were lowest in the Lake Border lacustrine sediment. Barium and titanium concentrations were highest in the Lake Border lacustrine sediment.

Elements occurring in concentrations exceeding 1 percent of the total mass in most samples include aluminum, calcium, iron, manganese, and potassium. These elements are the primary constituents of many rock-forming minerals. Concentrations of calcium, iron, and manganese were notably elevated in slag; potassium and sodium were relatively depleted. Trends similar to the slag analyses were observed in samples from the slag–aquifer interface, but concentrations generally were lower than slag. Calcium concentrations at the site were lowest in the Lake Border lacustrine sediment. Aluminum and potassium concentrations were highest in the Lake Border lacustrine sediment. By comparison, two sediment samples collected during 1995 from the southeastern corner of Lake George contained concentrations of antimony, arsenic, chromium, cobalt, iron, lead, manganese, nickel, vanadium, and zinc more than three times background levels (Roy F. Weston, Inc., 1995). Sediment from the southwestern corner of Lake George had no elevated constituent concentrations relative to background samples (Roy F. Weston, Inc., 1995). One sediment sample from the Lost Marsh had concentrations of arsenic, cadmium, cobalt, copper, iron, lead, nickel, selenium, thallium, vanadium, and zinc at concentrations more than three times greater than background (Roy F. Weston, Inc., 1995).

All elemental concentrations in aquifer samples from Bairstow Landfill were elevated relative to the sample of native sand unaffected by slag drainage. The sample of dune sand, which may have origins that are similar to the lacustrine Calumet aquifer sand, probably has undergone considerable reworking by sedimentary processes and has been exposed to surficial conditions that may have altered its geochemistry.

Figure 8 shows the X-ray diffractograms for five solid-phase samples, stacked according to depth, at BH-32 and BH-33. The intensities of the various X-ray peaks were assumed to indicate changing proportions of the minerals present. The stacked diffractograms indicate that quartz (SiO₂) is present at most depths but is most abundant in slag and least abundant in the Lake Border lacustrine sediment. The primary peak for calcite $(CaCO_3)$, $2\theta = 29.37^\circ$, indicates that quartz is present at all depths but is most abundant at the slag-aquifer interface. Dolomite (CaMg(CO₃)₂), primary peak at $2\theta = 30.94^\circ$, is similarly present at all depths and is most abundant in slag, least abundant at the slag-aquifer interface, and is present in substantial quantities in the sand immediately below the slag-aquifer interface.

Cristobalite (low temperature SiO_2), barian celestite (Ba_{0.25}Sr_{0.75}SO₄), and minrecordite (CaZn(CO₃)₂) are less abundant in all solid-phase samples than quartz, calcite, and dolomite. The

primary diffractogram peak of low-temperature cristobalite ($2\theta = 21.94^{\circ}$) indicates that small amounts of this mineral are in the slag samples and that it is less abundant in deeper samples. The primary and secondary diffractogram peaks for barian celestite overlap with the primary quartz and calcite peaks, making barian celestite difficult to distinguish. The identification of barian celestite was based on a prominent lower order peak at slightly more than $2\theta = 44.5^{\circ}$ but, because other lower-order peaks for celestite are not in the diffractogram for sample 32A, this identification is considered tentative.

The primary peak for minrecordite $(CaZn(CO_3)_2)$ overlaps the primary dolomite peak and cannot be identified in the solid-phase samples. The secondary and tertiary peaks, however, are clearly identified at about $2\theta = 50.75^{\circ}$ and 51.25° . Minrecordite may be present at all depths, but it is most abundant near the slag–sand interface.

Clay minerals can be an important geochemical consideration because of their cation-exchange capabilities. Clay minerals are not present in significant quantity in any solid-phase sample from the study site. Primary diffractogram peaks for clays generally occur at $2\theta < 20^{\circ}$; peak intensities in this region were subdued. It is possible that X-ray examination of a finer grain-size fraction would allow clay minerals to be identified. Clay minerals are considered to be allochthonous minerals and their presence nonindicative of secondary mineralization processes.

Figure 9 shows stacked diffractograms for a set of four solid-phase samples taken over approximately a 3-ft lakebed interval at BH-34SS. This sequence may be useful in describing geochemical changes occurring as ground water discharges into Lake George. Similar to the core samples at BH-32 and BH-33, quartz, dolomite, and calcite are the most abundant minerals in the lakebed samples. The stacked X-ray diffractograms may indicate that quartz abundance increases with depth, but calcite and dolomite abundances decrease with depth.



Cristobalite may be present in the two middledepth samples but only as a minor constituent. Minrecordite abundance increases with depth and is almost nonexistent in the shallowest lakebed sample.

A rock sample encrusted with a whitish precipitate from the southern shoreline of Lake George also was examined by X-ray diffraction. The mineralogy of the precipitate consisted predominantly of calcite, with minor quantities of quartz and dolomite and lesser quantities of barian celestite, manganese-bearing calcite, and minrecordite.

Mineral-Saturation Simulations

Constituents used in the WATEQFP calculations are identified in table 2 (back of report) and the calculated saturation indices are shown in table 4 (back of report). Saturation indices for 183 minerals were calculated; the minerals automatically were selected from the WATEQFP data base if the chemical components necessary to build the mineral had positive concentrations in the water-quality sample. For some water-quality-data sets, the saturation indices of some minerals were not calculated because concentrations of the necessary chemical constituents were less than reporting limits. Minerals with no calculated saturation index greater than 10^{-5} are omitted from table 4.

Calculated saturation indices show that many minerals are undersaturated in all water samples; these minerals are not thermodynamically favored to precipitate in the Bairstow Landfill groundwater system and may dissolve if present. Of 108 minerals shown in table 4 (back of report), 49 were undersaturated in all samples. Eleven of 108 minerals were supersaturated in all samples, and 46 minerals were supersaturated in some samples (table 4). Of the 46 minerals that occasionally are supersaturated, most indicate a tendency to precipitate in the Calumet aquifer and at site BH-34ND. Minerals were less frequently supersaturated in the four slag wells and in the sample from Lake George. The saturation states of minerals commonly identified in X-ray diffractograms for solid phase samples from Bairstow Landfill (including calcite, dolomite, quartz, and less commonly cristobalite) indicate a dependency on solution pH (fig. 10). The saturation indices of calcite and dolomite increase with pH, but the saturation indices of quartz and



EXPLANATION



- \times Cristobalite
- Dolomite
- ◇ Quartz



sample points was less than 9.9. The pH data and calculated mineral-saturation indices imply that silica forms would be dissolving in slag and precipitating in the shallow aquifer.

Several trace carbonate minerals, notably rhodochrosite ($MnCO_3$) and siderite (FeCO₃), also were undersaturated in the slag but were slightly undersaturated to slightly supersaturated in aquifer wells below the slag. These minerals were not present in quantities sufficient to be detected by the X-ray diffraction analyses but may be precipitation controls on manganese and iron concentrations in water.

The ability of WATEQFP to calculate accurately the tendency for a mineral to precipitate or

not part of the NETPATH data base and, because they were only detected infrequently and in relatively small abundances in X-ray diffractograms, they were not added to the NETPATH data base. Other phases that exist in the NETPATH data base were not considered in the Bairstow Landfill models because (1) they were not identified in the X-ray diffraction analyses, and (2) the relatively minute abundances of other minerals probably disqualifies them from having a major impact on the geochemical system.

Calcium, magnesium, and silica concentrations were used as constraints for the mass-balance models. Chloride was used as a fourth constraint of mixing proportions calculated for models where ground water from two wells combined to form the water quality observed at a third well. In all models, the situation's number of constraints equalled the degrees of freedom to obtain a unique solution.

The non-mixing mass-balance models indicated that slag drainage into the Calumet aquifer may precipitate calcite near the slag-aquifer interface (fig. 11). The simulated masses of calcite precipitated from solution, 4.92 and 5.69 millimoles per kilogram of water, as ground water moves from BH-31 to BH-32S and from BH-32SL to BH-33S. These mass transfers were large relative to others calculated for this model. The mass-balance models also indicated that calcite may be precipitating as ground water moves from the deeper aquifer (BH-32D) to the intermediatedepth aquifer (BH-33I) and as ground water flows horizontally, such as from BH-32I to BH-33I. The possibility that changes in concentrations of calcium and carbonate can be attributed to dilution of slag-contact ground water with less strongly affected ground water is addressed by the mixing mass-balance models. The calcite-rich precipitate observed along the Lake George shoreline confirms that some calcite precipitation is occurring; the mass transfer between BH-34SS and Lake George is 5.74 millimoles per kilogram of water.

The non-mixing mass-balance calculations indicate that dolomite is neither precipitating nor dissolving in significant quantities; mass transfers range from -1.56 to +1.13 millimoles per kilogram of water. The models indicate that dolomite dissolution may be occurring where ground water is flowing from slag into the shallow aquifer or across the ground-water/surface-water interface is dilution and dispersion of silica in the more dilute water of Lake George. Some combination of the two processes also may explain the observations.

Mass-balance models also were developed to evaluate the importance of ground-water mixing relative to concomitant mineral precipitation and dissolution to explain the observed changes in ground-water quality along the Bairstow Landfill flowpath. For example, the water quality at BH-32S alternately may be produced by mixing ground water from BH-31 and BH-32SL or by precipitating or dissolving calcite, dolomite, and silica.

Concentrations of chloride were used as a model constraint to determine the mixing proportions. Chloride is recognized as a conservative ion, and changes in concentration are likely attributable to ground-water mixing. Besides chloride, all other constraints (calcium, magnesium, and silica) and phases (calcite, dolomite, and SiO₂) remained the same as those used in the previously described non-mixing models.

The results of mixing mass-balance models are expressed as equations that relate mixing proportions of the two initial well chemistries to produce the water quality at the final downgradient well. Ground-water flowpaths determined from water-level data were used to select four potential mixing situations at the study site. Results of these models are presented in table 5.

Mixing model 1 explores the possibility that ground-water quality at well BH-32S is a result of combining water from BH-31 and BH-32SL (table 5). The calculations indicate that approximately 97 parts BH-31 ground water and 3 parts BH-32SL water plus calcite precipitation of 4.94 millimoles per kilogram of water and dissolution of dolomite and SiO₂ at 0.180 and 0.407 millimoles per kilogram of water, respectively, would yield the ground water observed at well BH-32S. These mass transfers are similar to the previously calculated two-component flow system from BH-31 to BH-32S. Mixing model 2 investigated the possibility that ground-water quality at well BH-32I is a result of mixing ground water from BH-31, BH-32S, and BH-32D; these flowpaths are indicated by water-level data. Model results indicate the water quality at BH-32I can be simulated by mixing about 11 parts of water from BH-31, 38 parts of water from BH-32S, and 51 parts of water from BH-32D, with a net dissolution of 0.186 and 0.304 millimoles per kilograms of water of dolomite and SiO₂, respectively.

Mixing model 3 attempted to explain the ground-water quality at well BH-33S by mixing water from wells BH-32S, BH-33SL, and BH-33I. A model could not be calculated based on the water-quality information measured in these wells. The high chloride concentration measured in water from well BH-33S was a limiting factor in calculating a satisfactory model. None of the initial ground-water compositions contained sufficient chloride to define the high chloride concentrations in BH-33S ground water.

Mixing model 4 derived the water quality from well BH-33I by mixing water from wells BH-32S, BH-32I, and BH-33S. Ground-water levels did not indicate flow from BH-32I to BH-33I, but horizontal flow of water with properties similar to BH-32I toward BH-33I may commonly occur. Results indicated that water quality at well BH-33I could be simulated by mixing about 1 part water from BH-32I with 99 parts water from BH-33S, dissolving 0.033 and 0.085 millimoles per kilogram of water of calcite and SiO₂, respectively, and precipitating 0.151 millimoles dolomite per kilogram of water. Calculations indicate that ground water at BH-33I did not require a contribution from well BH-32S. Water-level data did not indicate a significant component of flow from BH-33S to BH-33I, but the mixing model indicates that this may be the most common situation. Measurements of water levels were taken only on one occasion and may not represent all details of the prevalent flow regime.
Table 5. Geochemical mixing models and mass-transfer estimates along ground-water flowpaths at Bairstow Landfill, Hammond, Ind. [mmol/kg, millimoles per kilogram of water; SiO₂, quartz or cristobalite; --, not used or calculated]

Mixing model	Initial Well 1	Initial Well 2	Initial Well 3	Final Well	Simulated volume of water from initial well 1 in final well (percent)	Simulated volume of water from initial well 2 in final well (percent)	Simulated volume of water from initial well 3 in final well (percent)	Simulated mass transfer of calcite (mmol/kg)	Simulated mass transfer of dolomite (mmol/kg)	Simulated mass transfer of SiO ₂ (mmol/kg)
1	BH-31	BH-32SL		BH-32S	96.6	3.36		-4.94 ¹	0.180	0.407
2	BH-31	BH-32S	BH-32D	BH-32I	11.1	38.0	50.8	.000	.186	.304
3	BH-32S	BH-33SL	BH-33I	BH-33S	no models					
4	BH-32S	BH-32I	BH-33S	BH-33I	0.000	1.07	98.9	033	.151	085

¹Negative mass transfer indicates mineral precipitation from the dissolved solids in the mixed waters. Positive mass transfer indicates mineral dissolution contributing dissolved solids to the mixed waters.

No mixing combination could account for the chloride concentration in BH-33S because the value in that well exceeded the concentration in both wells immediately upgradient. Similarly, an appropriate mixing model could not be found by combining ground water at BH-34ND and BH-34SS to derive the water quality in the sample from Lake George because the chloride in the lake is higher than in both ground-water samples. Lake George likely has a source of chloride, such as from road-deicer-affected runoff, in addition to ground-water discharge.

Several situations can lead to inaccuracies in mass-balance models, including:

- selection of water-quality data from observation wells that are not along the same ground-water flowpath,
- 2) analytical mass-balance errors,
- 3) hydrodynamic dispersion in the aquifer,
- 4) departure from steady-state conditions,
- 5) significant and unaccounted recharge (dilution) or evaporation during the period that the ground water flows from the initial to final observation well, and
- 6) unknown or unquantified ion exchange and mineral impurities.

CHEMICAL CHARACTERISTICS OF SLAG-AFFECTED GROUND WATER

The statistical summary of the water-quality data identified properties and constituents that have been influenced by ground-water interaction with slag. Table 6 (back of report) presents calculated values of the total number of measurements in the data set, the median (middle) data value, the minimum and maximum values from the data set, and the first and third quartile (Q1 and Q3) that are the data values at the 25th and 75th positions of a hierarchical ordering of the data.

The statistical summary indicates that waterquality properties that generally are elevated in water from slag-contact wells include alkalinity, pH, and specific conductance. Alkalinity generally is elevated in water from slag-contact wells, relative to other ground-water settings, but not all slag-contact wells have high alkalinity values. Alkalinity values range from 24.9 to 884 mg/L in water from slag-contact wells, with a median of 279 mg/L. Almost all of the highest alkalinity values are from slag-contact wells; however, the highest alkalinity value in the data set was measured at a hazardous-waste-disposal site. The most consistently observed effect of slag on ground water is elevated pH. The pH values observed in water from 21 slag-contact wells ranged from 6.60 to 12.3, with median of 8.70. Water from slag-affected wells also has higher pH values, ranging from 6.9 to 9.90 than values in background water that ranged from 6.0 to 7.70. Specific conductance values, a bulk measure of dissolved solids, also are highest in water from slag-contact wells.

Numerous chemical elements can be elevated in slag-contact wells. Major ions with higher concentrations in water from slag-contact wells include calcium, potassium, sodium, chloride, and occasionally magnesium and sulfate. The median calcium concentration is more than three times greater in water from slag-contact wells than from background wells. The median potassium concentration in water from slag-contact wells (25.1 mg/L) was more than 20 times greater than from background wells. Potassium concentrations in water from slag-contact wells range from 3.12 to 170 mg/L. More than 75 percent of water samples from background wells contained less potassium than the lowest measured concentration in all slag-contact samples. The median sodium concentration in water from slag-contact wells is eight times greater than in background ground water, and the median chloride concentration in slagcontact wells (69 mg/L) is more than five times that of water from background wells. Magnesium

concentrations in slag-contact ground water vary the most, ranging from 0.010 to 211 mg/L, but the median value is about 5.0 mg/L less than the median concentration of water from slag-affected wells (22.8 mg/L). The median sulfate concentration in slag-contact wells is 190 mg/L, compared to 72 and 27.3 mg/L in slag-affected and background wells, respectively, but the highest measured value occurred in a slag-affected well.

Trace elements having higher concentrations in water from slag-contact wells include aluminum and barium and less frequently chromium, cobalt, copper, cyanide, manganese, mercury, nickel, and vanadium. The median aluminum concentration in slag-contact ground water is 49.7 µg/L compared to 23.5 and 23.5 μ g/L for water from slag-affected and background wells, respectively. The median barium concentration in slag-contact ground water is 128 μ g/L compared to 58.0 and 31.1 μ g/L for slag-affected and background ground water, respectively. Chromium, cobalt, copper, cyanide, manganese, nickel, and vanadium in slag-contact ground water have median concentrations that are about the same as slag-affected and background ground water. The range of chromium, cobalt, copper, cyanide, manganese, nickel, and vanadium concentrations in slag-contact ground water, however, is more variable than in slag-affected or background ground water; usually the maximum concentration is several times higher in water from slag-contact wells. For example, the median concentration of cyanide, a trace species, for all ground water is $10.0 \,\mu\text{g/L}$ (the minimum reporting limit) but the maximum concentrations for slagcontact, slag-affected, and background ground water are 212, 31.4, and 10.0 µg/L, respectively. Some trace elements or species like cyanide are not present in solid slag and may indicate possible disposal with industrial waste.

Total organic carbon (TOC) and suspendedsolids concentrations also are high in slag-contact ground water relative to slag-affected and background ground water. Concentrations of TOC in slag-contact samples range from 3.70 to 209 mg/L, with median value 15.1 mg/L, compared to concentrations of TOC in background ground water that range from <2.00 to 26.9 mg/L, with a median of 4.80 mg/L. Most ground water contains organic compounds in the form of humic and fulvic acids; however, high TOC concentrations in slag-contact ground water may indicate disposal of slag and human-affected organic compounds.

Suspended-solids concentrations in slagcontact ground water ranged from <3.00 to 5,310 mg/L, with a median value of 54.0 mg/L, compared to the range of <3.00 to 15.5 mg/L and the median of 3.0 mg/L in background ground water. High suspended-solids concentrations also may represent particulate oxides and hydroxides of aluminum, iron, and manganese (Hem, 1985, p. 60).

Although many ions are elevated in the slagcontact ground water, several chemical elements are more highly concentrated in slag-affected ground water. For example, arsenic concentrations in slag-affected ground water ranged from <1.70 to 55.0 μ g/L, while maximum values in slagcontact and background samples were 22.6 μ g/L and 12.8 μ g/L, respectively. The largest silica concentrations also were from slag-affected ground water.

Chemical elements not commonly detected in slag-contact wells include antimony, beryllium, cadmium, mercury, silver, and thallium. Lead is detected only randomly in any wells and may be present from atmospheric deposition. Zinc, also randomly detected, may represent industrial wastes deposited with slag. Zinc detections in background wells correspond to wells cased with galvanized steel.

CONCLUSIONS

Several conclusions can be drawn from this study of slag effects on aquifer geochemistry and ground-water quality:

(1) Concentrations of calcium, potassium, sodium, and sulfate were highest in water from wells screened partially or fully in slag. Potassium concentrations in ground water ranged from 2.9 to 120 mg/L, were highest in water from slag deposits, and decreased with depth. Silica concentrations were highest in wells screened directly beneath the slag-aquifer interface, and magnesium concentrations were highest in intermediate and deep aquifer wells. Silica concentrations in shallow and intermediate aquifer wells ranged from 27 to 41 mg/L and were about 10 times greater than those in water from slag deposits. The highest concentrations for aluminum, barium, molybdenum, nickel, and selenium were in the slag. The highest concentrations for chromium, lead, and zinc were in ground water from immediately below the slag-aquifer interface. Nitrite in ground-water from slag and ammonium in ground water from below the slag were the most abundant nutrients.

(2) Concentrations of several major ions and trace elements in water relate to pH values and bicarbonate concentrations and their effect on mineral-water interactions. For example, the samples with the largest concentrations in water of calcium, potassium, sodium, sulfate, aluminum, barium, molybdenum, nickel, and selenium, also have pH values ranging from 11.9 to 12.3 and are from slag wells. By comparison, water from wells with larger concentrations of silica and smaller concentrations of calcium also have smaller pH values. Water with the largest concentrations of chromium, lead, and zinc also generally have pH values that range from 9.0 to 9.9. Bicarbonate concentrations, as represented by alkalinity, are substantially greater in water from slag wells. Larger alkalinity values favor greater partial pressures of carbon dioxide and the dissolution of potassium and sodium aluminosilicate minerals (Stumm and Morgan, 1981, p. 545), possibly explaining the elevated potassium and sodium concentrations in slag-affected water.

(3) The concentrations of several chemical constituents and values of water-quality properties consistently are elevated in slag-contact ground water relative to regional background water quality; however, spuriously high values also can occur in slag-affected ground water. Consistently elevated water-quality properties in slag-contact wells included alkalinity, dissolved solids, suspended solids, total organic carbon, pH, and specific conductance. Major ions that consistently are elevated in slag-contact wells include calcium, potassium, sodium, chloride, and occasionally magnesium and sulfate. Trace elements having high concentrations in slag-contact wells include aluminum and barium and occasionally chromium, cobalt, copper, cyanide, manganese, mercury, nickel, and vanadium. Arsenic and silica concentrations generally are higher in slag-affected ground water than in slagcontact ground water.

(4) X-ray diffraction analyses of solid-phase samples indicate that the minerals calcite, dolomite, and quartz are relatively abundant and that barian celestite, cristobalite, manganese-bearing calcite, and minrecordite may occur infrequently.

(5) Of the 183 minerals examined with WATEQFP, 57 are supersaturated in at least one ground-water sample from Bairstow Landfill. Eleven minerals consistently were supersaturated, including calcite and dolomite. Quartz was not supersaturated in slag-contact wells, despite its abundance in X-ray diffractograms; both factors may indicate that quartz dissolution is a kinetically retarded process. Saturation indices for other minerals observed in X-ray diffractograms (barian celestite, cristobalite, and minrecordite) could not be calculated because the WATEQFP data base did not include the necessary thermodynamic information.

(6) Mass-balance models examined mass exchanges occurring along a ground-water flowpath at Bairstow Landfill. Results indicate that calcite precipitation is the dominant geochemical reaction where slag drainage enters the aquifer. Carbonate-mineral precipitation also may be occurring where slag drainage discharges to Lake George. Mass-balance models indicate that silica is dissolving where high-pH slag drainage enters the aquifer and continues to be an active process for some distance downgradient. Silica may be precipitating, probably as an amorphous form, where deeper ground water discharges to Lake George or concentrations of silica may be lowered in the lake as a result of dilution with lake water. Dolomite is dissolved in small quantities in all mixing massbalance models. The minerals minrecordite, barian celestine, and cristobalite were not included in the mass-balance models because their presence in solid-phase analyses was infrequent.

(7) Many chemical elements present in solid-

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SUPPLEMENTAL DATA

Table 2. Results of analyses of ground water and surface water from Bairstow Landfill, Hammond, Ind., August 1996

[USGS, U.S. Geological Survey; ^oC, degree Celsius; mg/L, milligram per liter; μ S/cm, microsiemens per centimeter at 25 degrees Celsius; CaCO₃, computed as calcium carbonate; --, no data; five-digit number in parentheses is WATSTORE (USGS) and usually the STORET (U.S.Environmental Protection Agency) parameter code; μ g/L, microgram per liter; <, less than]

				Temperature,
	USGS site			on site ¹
	identification	Date	Time	(°
Well name	number	sampled	sampled	

Table 2. Results of analyses of ground water and surface water from Bairstow Landfill, Hammond, Ind., August 1996—Continued

Well name	Date sampled	Time sampled	Calcium, dissolved ¹ (mg/L as Ca) (00915)	Magnesium, dissolved ¹ (mg/L as Mg) (00925)	Potassium, dissolved ¹ (mg/L as K) (00935)	Sodium, dissolved ¹ (mg/L as Na) (00930)	Chloride, dissolved ¹ (mg/L as Cl) (00940)	Fluoride, dissolved ¹ (mg/L as F) (00950)	Sulfate, dissolved ¹ (mg/L as SO ₄) (00945)	Silica, dissolved ¹ (mg/L as SiO ₂) (00955)
BH-31	08-15-96	1010	210	< 0.03	81	55	28	0.4	91	3.5
BH-32D	08-13-96	1255	88	41	2.9	34	19	.3	67	23
BH-32I	08-13-96	1117	83	27	3.7	50	24	.3	7.6	41
BH-32S	08-12-96	1645	20	3.6	19	170	29	1.1	6.7	28
BH-32S	08-13-96	940	21	4.4	20	170	29	1.0	6.5	26
BH-32S	08-13-96	1010	21	3.7	18	170	29	1.0	6.9	27
BH-32SL	08-12-96	1516	240	.01	120	170	53	.6	140	3.9

Well name	Date sampled	Time sampled	Nitrogen, ammonia, total ¹ (mg/L as N) (00610)	Nitrogen, nitrite, total ¹ (mg/L as N) (00615)	Nitrogen, ammonia+ organic, total (mg/L as N) (00625)	Nitrogen, nitrite +nitrate, total (mg/L as N) (00630)	Phosphorus, total (mg/L as P) (00665)	Phosphorus, ortho, total ¹ (mg/L as P) (70507)	Aluminum, dissolved ¹ (μg/L as Al) (01106)	Antimony, dissolved (μg/L as Sb) (01095)
BH-31	08-15-96	1010	1.7	2.9	2.6	3.1	< 0.01	< 0.01	180	<2
BH-32D	08-13-96	1255	2.6	.01	2.9	<.05	.08	.07	6	<1
BH-32I	08-13-96	1117	2.6	.01	2.7	<.05	.08	.11	8	<1
BH-32S	08-12-96	1645	7.1	.04	13	.07	.63	.52	80	<1
BH-32S	08-13-96	940	7.2	.04	13	.08	.50	.51	110	<1
BH-32S	08-13-96	1010	7.2	.03	13	.06	.54	.57	110	<1
BH-32SL	08-12-96	1516	2.0	1.1	3.4	1.1	.03	.01	820	<2
BH-33I	08-14-96	1510	12	.10	16	.19	.46	.47	30	<1
BH-33S	08-14-96	1345	13	.02	20	.07	.39	.36	160	<1
BH-33SL	08-14-96	1215	1.4	.74	2.6	.77	<.01	<.01	170	<2
BH-34ND	08-15-96	1220	3.4	.02	3.9	.10	.04	.04	20	<1
BH-34SS	08-13-96	1522	2.2	.40	3.4	.46	<.01	<.01	320	<2
Lake George	08-13-96	1620	.27	.04	.9	.10	<.01	<.01	50	11

Table 2. Results of analyses of ground water and surface water from Bairstow Landfill, Hammond, Ind., August 1996-Continued

Well name	Date sampled	Time sampled	Arsenic, dissolved (μg/L as As) (01000)	Barium, dissolved ¹ (µg/L as Ba) (01005)	Beryllium, dissolved (µg/L as Be) (01010)	Cadmium, dissolved ¹ (μg/L as Cd) (01025)	Chromium, dissolved ¹ (μg/L as Cr) (01030)	Cobalt, dissolved ¹ (µg/L as Co) (01035)	Copper, dissolved ¹ (µg/L as Cu) (01040)	Iron, dissolved ¹ (μg/L as Fe) (01046)
BH-31	08-15-96	1010	<1	180	<2	<2	<2	<2	<2	290
BH-32D	08-13-96	1255	55	200	<1	<1	<1	<1	<1	2,600
BH-32I	08-13-96	1117	7	180	<1	<1	4	1	<1	2,500
BH-32S	08-12-96	1645	15	40	<1	<1	5	<1	<1	240
BH-32S	08-13-96	940	19	44	<1	<1	4	<1	3	360
BH-32S	08-13-96	1010	18	45	<1	<1	2	<1	2	230
BH-32SL	08-12-96	1516	<1	410	<2	<2	<2	<2	<2	12
BH-33I	08-14-96	1510	19	41	<1	<1	2	<1	3	510
BH-33S	08-14-96	1345	43	24	<1	<1	3	<1	1	870
BH-33SL	08-14-96	1215	<1	220	<2	<2	<2	<2	3	91
BH-34ND	08-15-96	1220	8	24	<1	<1	<1	<1	<1	34
BH-34SS	08-13-96	1522	1	320	<2	<2	<2	<2	<2	160
Lake George	08-13-96	1620	3	41	<1	<1	<1	<1	2	74

Table 2. Results of analyses of ground water and surface water from Bairstow Landfill, Hammond, Ind., August 1996—Continued

Well name	Date sampled	Time sampled	Lead, dissolved ¹ (µg/L as Pb) (01049)	Manganese, dissolved ¹ (µg/L as Mn) (01056)	Molybdenum, dissolved ¹ (μg/L as Mo) (01060)	Nickel, dissolved ¹ (μg/L as Ni) (01065)	Selenium, dissolved ¹ (μg/L as Se) (01145)	Silver, dissolved ¹ (µg/L as Ag) (01075)	Uranium, dissolved ¹ (μg/L as U) (22703)	Zinc, dissolved ¹ (μg/L as Zn) (01090)
BH-31	08-15-96	1010	<2	<2	58	9	4	<2	<2	2
BH-32D	08-13-96	1255	<1	97	2	3	<1	<1	<1	3
BH-32I	08-13-96	1117	<1	130	9	4	<1	<1	<1	3
BH-32S	08-12-96	1645	5	25	35	3	<1		<1	8
BH-32S	08-13-96	940	10	45	34	4	<1	<1	<1	14
BH-32S	08-13-96	1010	3	48	35	5	<1	<1	<1	14
BH-32SL	08-12-96	1516	<2	<2	170	9	2	<2	<2	2
BH-33I	08-14-96	1510	12	48	120	4	2	<1	<1	11
BH-33S	08-14-96	1345	15	23	80	6	<1	<1	<1	28
BH-33SL	08-14-96	1215	<2	<2	160	13	4	<2	<2	3
BH-34ND	08-15-96	1220	<1	2	160	2	2	<1	<1	5
BH-34SS	08-13-96	1522	<2	<2	200	13	3		<2	2
Lake George	08-13-96	1620	2	5	120	2	<1	<1	<1	3

Table 2. Results of analyses of ground water and surface water from Bairstow Landfill, Hammond, Ind., August 1996-Continued

Well name	Date sampled	Time sampled	Hardness, total (mg/L as CaCO ₃) (00900)	Solids, residue at 180°C, total ¹ (mg/L) (70300)	Solids, sum of constituents, dissolved (mg/L) (70301)	Analytical charge imbalance (percent)
BH-31	08-15-96	1010		848		+4.97
BH-32D	08-13-96	1255	390	527	519	-2.88
BH-32I	08-13-96	1117	320	506	500	-1.82
BH-32S	08-12-96	1645	65	634	555	
BH-32S	08-13-96	940	71	588	565	-1.41
BH-32S	08-13-96	1010	68	624	560	
BH-32SL	08-12-96	1516	600	1,240	1,270	-15.9
BH-33I	08-14-96	1510	56	680	629	-5.75
BH-33S	08-14-96	1345	28	864	785	-3.66
BH-33SL	08-14-96	1215		1,230		-10.4
BH-34ND	08-15-96	1220	47	581	551	-6.50
BH-34SS	08-13-96	1522		1,060		-15.4
Lake George	08-13-96	1620	87	433	423	-4.31

Table 2. Results of analyses of ground water and surface water from Bairstow Landfill, Hammond, Ind., August 1996-Continued

¹Denotes water-quality property used in WATEQFP mineral-saturation calculations.

 2 Redox-potential value reported relative to the calomel electrode.

 $[percent, percent of total sample mass; ppm, parts per million; <, less than; \mu m, micrometers] \\$

Sample identifier	Lithology	Aluminum (percent)	Antimony (ppm)	Arsenic (ppm)	Barium (ppm)	Beryllium (ppm)	Bismuth (ppm)	Cadmium (ppm)
32A	Calumet aquifer	4.22	<5	5	267	2	<5	<0.4
32B	Calumet aquifer	4.66	<5	<5	291	2	<5	<.4
33D	Calumet aquifer	5.25	<5	6	302	2	<5	<.4
33C	Slag-Calumet aquifer interface	4.20	<5	8	317	2	<5	.7
33A	Slag	2.47	<5	<5	324	3	<5	1.9
33B	Slag	2.56	<5	<5	265	2	<5	.9
32C <2µm	Lake Border sequence lacustrine sediment	9.99	<5	<5	451	3	<5	<.4
32C 2–5µm	Lake Border sequence lacustrine sediment	8.22	7	<5	513	2	<5	<.4
32C 5-20µm	Lake Border sequence lacustrine sediment	7.19	<5	<5	463	2	<5	<.4
34A	Lakebed sediment	1.46	13	5	135	1	<5	3.3
34B	Lakebed sediment	2.53	7	<5	261	<1	<5	<.4
34C	Lakebed sediment	2.16	17	12	269	2	<5	3.8
34D	Lakebed sediment	3.81	<5	<5	260	1	<5	<.4
34E	Lakebed sediment	4.87	<5	<5	274	2	<5	<.4
34E replicate	Lakebed sediment	4.64	<5	<5	264	1	<5	<.4
Dune sand	Dune sand	1.94	<5	<5	325	<1	<5	<.4

Sample identifier	Lithology	Calcium (percent)	Chromium (ppm)	Cobalt (ppm)	Copper (ppm)	Gold (ppm)	Iron (percent)	Lanthium (ppm)
32A	Calumet aquifer	11.05	1,268	19	65	<4	4.87	22
32B	Calumet aquifer	10.39	929	16	74	<4	4.41	23
33D	Calumet aquifer	10.71	1,403	23	81	<4	4.97	26
33C	Slag-Calumet aquifer interface	12.99	892	13	139	<4	5.72	22
33A	Slag	16.98	2,789	10	117	<4	11.4	22
33B	Slag	14.28	2,106	5	105	<4	10.0	19
32C <2µm	Lake Border sequence lacustrine sediment	4.49	111	17	40	<4	4.70	38
32C 2–5µm	Lake Border sequence lacustrine sediment	6.81	123	10	54	<4	3.78	38
32C 5–20µm	Lake Border							

Sample identifier	Lithology	Lead (ppm)	Manganese (ppm)	Molybdenum (ppm)	Nickel (ppm)	Niobium (ppm)	Phosphorous (percent)
32A	Calumet aquifer	58	5,121	13	467	6	0.133
32B	Calumet aquifer	57	4,319	12	335	6	.084
33D	Calumet aquifer	55	3,643	15	531	6	.053
33C	Slag-Calumet aquifer interface	133	6,919	12	208	8	.096
33A	Slag	116	25,109	20	295	18	.294
33B	Slag	117	23,754	11	165	18	.212
32C <2µm	Lake Border sequence lacustrine sediment	26	492	3	56	4	.051
32C 2–5µm	Lake Border sequence lacustrine sediment	35	808	3	51	9	.048
32C 5–20μm	Lake Border sequence lacustrine sediment	33	465	3	42	7	.031
34A	Lakebed sediment	402	4,990	12	87	4	.059
34B	Lakebed sediment	16	597	3	77	2	.023
34C	Lakebed sediment	587	10,042	31	250	6	.083
34D	Lakebed sediment	147	2,147	19	562	4	.035
34E	Lakebed sediment	68	771	8	128	4	.033
34E replicate	Lakebed sediment	67	731	7	125	4	.032
Dune sand	Dune sand	8	193	<2	12	2	.0107

Sample	Lithology	Potassium	Scandium	Silver	Sodium	Strontium	Thorium	Tin
identifier	Littology	(percent)	(ppm)	(ppm)	(percent)	(ppm)	(ppm)	(ppm)
32A	Calumet aquifer	1.90	9	0.6	0.29	107	6	6
32B	Calumet aquifer	2.03	9	<.5	.42	119	6	5
33D	Calumet aquifer	2.17	10	.5	.38	111	7	12
33C	Slag-Calumet aquifer interface	1.63	9	1.2	.39	176	6	26
33A	Slag	.21	6	1.3	.10	151	6	13
33B	Slag	.33	6	.8	.14	180	5	11
32C <2µm	Lake Border sequence lacustrine sediment	3.63	18	1.0	.72	210	14	4
32C 2–5µm	Lake Border sequence lacustrine sediment	3.30	14	1.1	.49	168	11	19
32C 5–20μm	Lake Border sequence lacustrine sediment	3.01	12	<.5	.47	136	6	14
34A	Lakebed sediment	.41	3	.5	.21	663	2	34
34B	Lakebed sediment	1.33	4	<.5	.63	123	2	<2
34C	Lakebed sediment	.63	5	.8	.20	356	4	42
34D	Lakebed sediment	1.92	8	<.5	.38	108	5	15
34E	Lakebed sediment	2.51	9	.6	.45	204	7	14
34E replicate	Lakebed sediment	2.43	9	<.5	.44	197	6	13
Dune sand	Dune sand	1.26	3	<5	.50	89	<2	<2

Sample identifier	Lithology	Titanium (percent)	Tungsten (ppm)	Uranium (ppm)	Vanadium (ppm)	Yttrium (ppm)	Zinc (ppm)	Zirconium (ppm)
32A	Calumet aquifer	0.24	7	<10	158	18	152	47
32B	Calumet aquifer	.26	16	10	142	18	148	52
33D	Calumet aquifer	.26	6	<10	119	21	170	53
33C	Slag-Calumet aquifer interface	.24	32	<10	166	21	266	44
33A	Slag	.25	17	<10	336	25	526	38
33B	Slag	.30	13	<10	304	21	486	48
32C <2µm	Lake Border sequence lacustrine sediment	.34	8	19	163	26	101	83
32C 2–5µm	Lake Border sequence lacustrine sediment	.45	4	18	129	23	95	64
32C 5–20µm	Lake Border sequence lacustrine sediment	.36	<4	<10	103	17	78	55
34A	Lakebed sediment	.10	8	<10	79	11	889	23
34B	Lakebed sediment	.11	<4	15	30	9	52	22
34C	Lakebed sediment	.15	12	<10	129	16	1,046	31
34D	Lakebed sediment	.21	<4	<10	84	17	231	48
34E	Lakebed sediment	.24	<4	<10	84	18	149	55
34E replicate	Lakebed sediment	.23	<4	<10	80	17	147	51
Dune sand	Dune sand	.11	<4	<10	20	7	11	30

Table 4. Mineral-saturation indices calculated for water samples from Bairstow Landfill, Hammond, Ind.

[Bold type, positive saturation indices; Shaded rows, minerals present in X-ray diffraction analyses; --, not caluclated because constituent concentrations were less than laboratory reporting limits]

	Well Name										
Mineral name	BH-31	BH-32SL	BH-32S	BH-32I	BH-32D	BH33-SL	BH-33S	BH-33I	BH-34SS	BH-34ND	Lake George
Adularia KAlSi ₃ O ₈	-6.13	-5.62	2.31	1.23	0.21	-6.13	2.55	1.83	-6.25	2.00	1.45
Albite Na(Si ₃ Al)O ₈	-8.78	-7.97	.76	10	-1.18	-8.44	.48	.27	-8.61	28	-3.48
Allophane (a) $[Al(OH)_3]_{(1-x)}$ $[SiO_2]_x$	-3.17	-2.37	76	05	31	-3.72	-1.38	-1.09	-3.75	-3.22	-1.69
Allophane (P) [Al(OH) ₃] _(1-x) [SiO ₂]A67 w	3.j ET 2 n	n									

	Well Name										
Mineral name	BH-31	BH-32SL	BH-32S	BH-32I	BH-32D	BH33-SL	BH-33S	BH-33I	BH-34SS	BH-34ND	Lake George
Ba ₃ (AsO ₄) ₂			13.8	14.8	10.8		12.1	10.9	11.4		8.36
Barite BaSO ₄	.58	.74	99	31	.59	.59	91	26	41	28	02
Beidellite (Ca, Na) _{0.3} Al ₂ (OH) ₂ -(Al, Si) ₄ O_{10} (H ₂ O) ₄	-14.4	-13.3	2.21	4.60	3.13	-14.2	.72	1.62	-14.2	-1.29	-2.20
Bixbyite γ-AlO [.] OH			-13.6	-18.0	-18.2		-13.1	-13.7		-9.08	-4.52
Boehmite γ-AlO(OH)	-2.96	-2.43	37	.47	.23	-2.91	79	597	-2.81	-1.94	31
Brucite Mg(OH) ₂		37	-2.83	-5.92	-5.53		-3.48	-3.53		-1.56	-3.37
Bunsenite NiO	-2.18	-2.34	-5.56	-4.15	-7.14	-1.74	-5.21	-5.75	-1.55	-4.59	-5.24
Calcite CaCO ₃	2.62	2.95	1.55	.33	.43	2.99	1.51	1.17	2.95	1.50	.64
Cerrusite PbCO ₃			-1.83				-2.14	-1.56		-1.54	-2.23
CaSeO ₃	-4.73	-5.59				-5.16		-6.00	-5.28	-6.13	
Chalcedony SiO ₂	-2.84	-2.93	.24	.51	.25	-2.77	.08	.26	-2.84	.31	82

Table 4. Mineral-saturation indices calculated for water samples from Bairstow Landfill, Hammond, Ind.-Continued

									_		
Mineral name	BH-31	BH-32SL	BH-32S	BH-32I	BH-32D	BH33-SL	BH-33S	BH-33I			
Chlorite 14A Mg ₅ Al(Si ₃ Al) $O_{10}(OH)_8$		7.51	8.83	-4.11	-3.43		4.14	4.84		11.6	2.14
Chlorite 7A Mg ₅ Al(Si ₃ Al) O ₁₀ (OH) ₈		4.04	5.35	-7.59	-6.90		.69	1.38		8.27	-1.19
Chrysotile Mg ₃ [Si ₂ O ₅] (OH) ₄		4.81	3.76	-4.96	-4.32		1.40	1.62		7.23	73
Clinoenstatite (Mg,Fe ⁺²)[SiO ₃]		-1.29	58	-3.40	-3.27		-1.40	-1.27		.70	-2.27
Clpyromorphite Pb ₅ (PO ₄) ₃ Cl			-4.33				-6.68	-1.88		-4.88	
Cristobalite SiO ₂	-2.78	-2.87	.29	.56	.31	-2.72	.13	.31	-2.80	.34	79
Copper Cu (metal)			1.67			-3.15	1.33	.99			-9.34
Cu(OH) ₂			-2.74			-2.50	-3.12	-2.73			-2.38
Cupric Ferrite CuFe ₂ O ₄			13.6			8.44	13.8	13.8			13.2
Cuprite Cu ₂ O			3.15			-1.46	2.41	2.47			-7.59

Well Name

Table 4. Mineral-saturation indices calculated for water samples from Bairstow Landfill, Hammond, Ind.-Continued

	Well Name										
Mineral name	BH-31	BH-32SL	BH-32S	BH-32I	BH-32D	BH33-SL	BH-33S	BH-33I	BH-34SS	BH-34ND	Lake George
Cuprous Ferrite CuFeO ₂			16.6			11.5	16.5	16.4			10.7
Diaspore α-AlO(OH)	-1.16	63	1.42	2.27	2.02	-1.16	.98	1.18	-1.07	22	1.36
Diopside Ca(Mg,Fe) [Si ₂ O ₆]		4.52	2.21	-3.54	-3.44		1.76	.77		4.71	-1.53
Dioptase Cu ₆ (SiO ₁₈) ⁻ 6H ₂ O			-3.87			-6.66	-4.42	-3.84			-4.63
Dolomite (d) CaMg(CO ₃) ₂		1.16	2.10	21	.15		.84	1.41		2.08	.63
Dolomite (c) CaMg(CO ₃) ₂		1.76	2.69	.37	.74		1.43	2.00		2.64	1.16
Epsomite MgSO ₄ ·7H ₂ O		-8.36	-6.23	-5.32	-4.24		-7.48	-5.46		-5.41	-4.79
FCO ₃ Apatite Ca _{9.49} Na _{.36} Mg _{.14} (PO ₄) _{4.8} (CO ₃) _{1.2} F _{2.48}		21.9	22.7	12.2	12.7		19.4	20.0		15.9	
Fe ₃ (OH) ₈	-2.75	-6.79	6.24	.05	.35	-4.94	6.98	6.00	-5.36	96	-1.70
Fe(OH) _{2.7} Cl _{0.3}	3.34	1.88	6.43	4.96	4.95	2.80	6.61	6.68	2.74	4.71	5.99

Table 4. Mineral-saturation indices calculated for water samples from Bairstow Landfill, Hammond, Ind.-Continued

Fluorapatite $Ca_5(PO_4)_3F$		4.36	5.53	0.09	0.38		3.97	4.27		2.32	
Fluorite CaF ₂	-1.56	-1.71	-1.60	-1.89	-1.92	-1.31	-2.41	-1.76	-1.69	-2.28	-1.76
Forsterite MgSiO ₄		-1.82	-3.58	-9.49	-8.96		-5.03	-4.96		98	-5.75
Gibbsite (c) Al(OH) ₃	-2.35	-1.81	.24	1.08	.84	-2.37	20	.00	-2.29	-1.45	.11
Goethite α-FeO [·] OH	5.91	4.40	8.15	6.11	6.15	5.23	8.38	8.17	5.22	6.50	7.33

Greenalite

(Fe,Mg)₃

Hydrocerrusite Pb ₃ (CO ₃) ₂ (OH) ₂	 	-5.83	-2.25		 -6.21	-5.43	 -3.79	-7.12
Hydroxyapatite Ca ₅ (PO ₄) ₃ (OH,F,Cl)	 6.63	4.65		-1.83	 3.78	3.10	 2.46	
Illite $K_{1-1.5}Al_4[Si_{7-}]_{6.5}Al_{1-1.5}O_{20}]$ (OH) ₄	 -10.1							

	Well Name										
Mineral name	BH-31	BH-32SL	BH-32S	BH-32I	BH-32D	BH33-SL	BH-33S	BH-33I	BH-34SS	BH-34ND	Lake George
Malachite Cu ₂ (OH) ₂ CO ₃			-4.62			-8.45	-5.95	-4.20			-3.80
Manganite MnO [.] OH			-6.08	-8.27	-8.39		-5.98	-6.25		-4.55	-2.68
MnHPO ₄			52	.27	.10		-1.40	14		-3.29	
$\begin{array}{l} Montmorillonite BF\\ Al_2Si_4O_{10}(OH)_2\\ xH_2O \end{array}$		-9.90	5.00	4.97	3.64		4.05	4.60		3.63	1.28
$\begin{array}{c} Montmorillonite \ AB \\ Al_2Si_4O_{10}(OH)_2 \\ xH_2O \end{array}$		-9.42	4.93	4.06	2.84		3.93	4.41		3.59	.91
$\begin{array}{c} \text{Montmorillonite CA} \\ \text{Al}_2\text{Si}_4\text{O}_{10}(\text{OH})_2 \\ \text{xH}_2\text{O} \end{array}$	-14.4	-13.5	1.89	4.33	2.84	-14.2	.36	1.29	-14.3	-1.56	-2.43
$\begin{array}{c} Muscovite \\ K_2Al_4 \\ [Si_6Al_2O_{20}] \\ (OH,F)_4 \end{array}$	-5.28	-3.70	8.35	8.96	7.44	-5.30	7.70	7.38	-5.25	4.70	4.40
Nahcolite NaHCO ₃	-6.78	-5.65	-3.69	-4.23	-4.41	-5.57	-3.62	-3.61	-5.92	-4.45	-4.53
Nantokite CuCl			-4.78			-9.58	-5.34	-4.39			-9.12

 Table 4. Mineral-saturation indices calculated for water samples from Bairstow Landfill, Hammond, Ind.—Continued

	Well Name										
Mineral name	BH-31	BH-32SL	BH-32S	BH-32I	BH-32D	BH33-SL	BH-33S	BH-33I	BH-34SS	BH-34ND	Lake George
Natron Na ₂ CO ₃ ·10H ₂ O	-6.61	-4.94	-5.82	-8.89	-9.15	-5.48	-5.20	-6.13	-5.95	-6.51	-8.14
Nesquehonite MgCO3 [.] 3H ₂ O		-4.13	-1.79	-2.89	-2.63		-3.03	-2.12		-1.85	-2.47
Ni(OH) ₂	.92	.75	-2.46	-1.04	-4.10	.58	-2.39	-2.86	.50	-2.74	-4.05
Ni ₂ SiO ₄	14	55	-3.81	72	-6.96	.67	-3.31	-4.20	.93	-2.03	-4.59
$Pb(OH)_2(c)$			-1.62				-1.36	-1.74		06	-1.97
PbSiO ₃			-4.10				-3.99	-4.20		-2.47	-5.52
Phillipsite (0.5Ca,Na,K) ₃	-7.63	-6.97	1.36	.39	62	-7.05	1.49	.99	-7.06	1.34	-1.64
[Al ₃ Si ₅ O ₁₆] [.] 6H ₂ O											
Portlandite Ca(OH) ₂	-2.05	-2.31	-8.51	-11.7	-11.47	-2.56	-7.91	-9.22	-2.21	-7.05	-9.01
$\begin{array}{c} \text{Prehnite} \\ \text{Ca}_2\text{Al}[\text{AlSi}_3\text{O}_{10}] \\ \text{(OH)}_2 \end{array}$.70	.98	2.22	-1.69	-2.49	41	1.95	.30	.11	1.53	-2.91
Pyrochroite Mn(OH) ₂			-4.21	-6.46	-6.41		-4.00	-4.66		-4.72	-5.95
Pyrolusite MnO ₂			-15.6	-17.7	-17.9		-15.2	-15.2		-10.5	-4.75

Table 4. Mineral-saturation indices calculated for water samples from Bairstow Landfill, Hammond, Ind.-Continued

Table 4. Mineral-saturation indices calculated for	r water samples from F	Bairstow Landfill, Hammon	d. Ind.—Continued
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Well Name

Mineral name	BH-31	BH-32SL	BH-32S	BH-32I	BH-32D						
$\begin{array}{c} Pyrophyllite \\ Al_4[Si_8O_{20}] \\ (OH)_4SiO_2 \end{array}$	12.6	-11.9	4.89	7.67	6.22	-11.5	3.67	4.73	-11.4	3.12	2.40
Quartz SiO ₂	-2.38	-2.47	.70	.97	.71	-2.32	.54	.72	-2.40	.74	41
Rhodochrosite (d) MnCO ₃			61	87	93		89	61		-1.96	-1.74
Rhodochrosite (c) MnCO ₃			.08	17	23		18	.09		-1.22	99
Sepiolite (d) $Mg_4(OH)_2Si_6O_{15}$ $\cdot H_2O+4H_2O$		-4.10	.48	-4.87	-4.91		-1.48	-1.00		2.32	-5.20
Sepiolite (c) $Mg_4(OH)_2Si_6O_{15}$ H_2O+4H_2O		-1.49	3.10	-2.26	-2.28		1.18	1.65		5.18	-2.21
Siderite (d) FeCO ₃	-9.29	-9.73	.62	.50	.60	-8.83	.42	.79	-9.46	-4.12	-5.07
Siderite (c) FeCO ₃	-8.92	-9.35	.99	.88	.97	-8.42	.81	1.17	-9.04	-3.69	-4.61
Silica gel	-3.38	-3.47	30	02	28	-3.30	45	27	-3.38	22	-1.35
SiO ₂ (a)	-3.72	-3.81	63	36	62	-3.62	78	60	-3.69	53	-1.65
Smithsonite ZnCO ₃	-9.06	-8.62	-3.44	-3.26	-3.21	-7.24	-3.66	-3.21	-7.72	-3.99	-3.04

	Well Name										
Mineral name	BH-31	BH-32SL	BH-32S	BH-32I	BH-32D	BH33-SL	BH-33S	BH-33I	BH-34SS	BH-34ND	Lake George
Strengite Fe ³⁺ (PO ₄) [.] 2H ₂ O		-16.8	-3.40	-2.39	-2.55		-4.22	-2.52		-7.18	
$\begin{array}{c} \text{Talc} \\ \text{Mg}_6[\text{Si}_8\text{O}_{20}] \\ \text{(OH)}_4 \end{array}$		2.49	7.80	38	25		5.15	5.72		11.5	1.35
Tenorite CuO			-1.72			-1.48	-2.10	-1.71			-1.36
Tremolite Ca ₂ Mg ₅ Si ₈ O ₂₂ (OH) ₄		16.5	17.2	-2.48	-2.16		13.6	12.2		25.6	2.77
Vivianite Fe ₃ (PO ₄) ₂ [.] 8H ₂ O		-37.3	-1.30	-1.52	-1.34		-2.58	48		-17.3	
Wairakite CaAl ₂ Si ₄ O ₁₂ 2H ₂ O	-11.9	-11.5	89	-1.32	-2.61	-12.2	-1.81	-1.99	-11.9	-2.51	-5.89
Willemite ZnSiO ₄	-5.85	-6.26	-2.32	-5.67	-5.59	-4.33	-1.80	-2.65	-4.74	-1.00	-2.77
Witherite BaCO ₃	64	.17	-1.36	-2.69	-2.60	20	-1.28	-1.74	93	-1.60	-2.62
Zincite (c) ZnO	-3.28	-3.44	-3.05	-4.86	-4.69	-2.51	-2.70	-3.22	-2.67	-2.36	-2.65
$Zn(OH)_2(e)$	-3.05	-3.21	-2.83	-4.64	-4.50	-2.60	-2.59	-3.08	-2.86	-2.64	-3.19
$Zn(OH)_2(c)$	-3.75	-3.91	-3.53	-5.34	-5.20	-3.30	-3.29	-3.78	-3.56	-3.34	-3.89

 Table 4. Mineral-saturation indices calculated for water samples from Bairstow Landfill, Hammond, Ind.—Continued

	Well Name										
Mineral name	BH-31	BH-32SL	BH-32S	BH-32I	BH-32D	BH33-SL	BH-33S	BH-33I	BH-34SS	BH-34ND	Lake George
$Zn(OH)_2(g)$	-3.26	-3.42	-3.04	-4.85	-4.71	-2.81	-2.80	-3.29	-3.07	-2.85	-3.40
$Zn(OH)_2(b)$	-3.30	-3.46	-3.08	-4.89	-4.75	-2.85	-2.84	-3.33	-3.11	-2.89	-3.44
$Zn(OH)_2(a)$	-4.00	-4.16	-3.78	-5.59	-5.45	-3.55	-3.54	-4.03	-3.81	-3.59	-4.14
ZnCO ₃ ·H ₂ O	-8.68	-8.25	-3.06	-2.88	-2.84	-6.92	-3.31	-2.85	-7.43	-3.71	-2.81
ZnO (a)	-2.86	-3.02	-2.64	-4.45	-4.31	-2.41	-2.40	-2.89	-2.67	-2.45	-3.00
ZnSiO ₃	-1.49	-1.74	1.81	.27	.18	64	2.01	1.67	86	2.59	1.19

Table 4. Mineral-saturation indices calculated for water samples from Bairstow Landfill, Hammond, Ind.-Continued

Table 6. Statistical summary of ground-water-quality data from Bairstow Landfill and from the Grand Calumet aquifer,Hammond, Ind.

 o C, degrees Celsius; mv, millivolts; mg/L, milligrams per liter; μ S/cm, microsiemens per centimeter at 25 degrees Celsius; CaCO₃, computed as calcium carbonate; μ g/L, micrograms per liter, <, less than]

Water-quality property	Well type	Number of samples	Minimum value	1st quartile	Median	3rd quartile	Maximum value
Temperature (^o C)	Slag-contact	21	11.9	14.1	15.0	16.4	22.0
	Slag-affected	25	11.6	12.8	14.5	16.0	23.5
	Background	11	10.3	11.2	12.0	14.0	14.8
pH (standard units)	Slag-contact	21	6.60	7.50	8.70	11.5	12.3
	Slag-affected	19	6.90	7.30	7.50	8.00	9.90
	Background	11	6.00	6.80	7.30	7.40	7.70
Redox potential (mv)	Slag-contact	21	-446	-195	-64.0	84.5	134
	Slag-affected	25	-183	-134	-100	-1.00	136
	Background	11	-198	-163	-78.0	5.00	52.0
Dissolved oxygen (mg/L)	Slag-contact	19	.10	.30	.60	1.40	4.20
	Slag-affected	22	<.10	.10	.20	1.45	6.30
	Background	11	<.10	.10	.20	.30	6.10
Specific conductance (µS/cm)	Slag-contact	21	192	930	1,880	3,820	5,720
	Slag-affected	26	186	469	847	1,300	3,480
	Background	11	164	239	445	900	1,190
Alkalinity (mg/L as CaCO ₃)	Slag-contact	20	24.9	153	279	661	884
	Slag-affected	25	74.6	177	207	399	532
	Background	11	41.8	95.5	163	216	279

Table 6. Statistical summary of ground-water-quality data from Bairstow Landfill and from the Grand Calumet aquifer,

 Hammond, Ind.—Continued

Calcium (mg/L)	Slag-contact	21	10.4	121	189	245	445
	Slag-affected	25	9.18	53.7	83.0	132	514
	Background	11	10.7	27.0	54.2	60.0	301
Magnesium (mg/L)	Slag-contact	21	.01	.09	17.6	60.0	211
	Slag-affected	25	.12	6.71	22.8	35.6	68.4
	Background	11	5.03	8.63	14.4	26.4	50.6

Table 6. Statistical summary of ground-water-quality data from Bairstow Landfill and from the Grand Calumet aquifer
Hammond, Ind.—Continued

Water-quality property	Well type	Number of samples	Minimum value	1st quartile	Median	3rd quartile	Maximum value
Silica (mg/L)	Slag-contact	20	3.10	10.0	17.0	28.7	35.3
	Slag-affected	25	9.60	17.5	25.3	32.6	74.0
	Background	11	10.5	12.2	12.6	13.4	29.7
Ammonia (mg/L)	Slag-contact	20	.10	1.02	2.40	8.80	44.3
	Slag-affected	24	.10	.10	1.30	3.38	90.3
	Background	11	.10	.30	.32	.90	2.60
Aluminum (µg/L)	Slag-contact	21	20.9	23.5	49.7	251	820
	Slag-affected	25	6.00	20.9	23.5	36.7	160
	Background	11	20.9	20.9	23.5	74.9	383
Antimony (µg/L)	Slag-contact	21	<2.00	<15.7	<15.7	<17.9	<17.9
	Slag-affected	25	<1.00	<8.35	<15.7	<17.9	<17.9
	Background	11	<15.7	<15.7	<17.9	<17.9	<17.9
Arsenic (µg/L)	Slag-contact	21	<1.00	<1.70	2.70	5.00	22.6
	Slag-affected	25	<1.70	<1.70	3.60	18.8	55.0
	Background	11	<1.70	<1.70	1.90	3.30	12.8
Barium (µg/L)	Slag-contact	21	30.2	56.3	128	284	690
	Slag-affected	25	10.7	25.0	58.0	134	410
	Background	11	14.7	16.5	31.1	83.0	229

Water-quality property	Well type	Number of samples	Minimum value	1st quartile	Median	3rd quartile	Maximum value
Beryllium (µg/L)	Slag-contact	21	<.50	<.50	<1.20	<1.20	2.00
	Slag-affected	25	<.50	<.50	<1.00	<1.20	<1.20
	Background	11	<.50	<.50	<.50	<1.20	<1.20
Cadmium (µg/L)	Slag-contact	21	<1.50	<1.50	<1.50	<1.70	2.00
	Slag-affected	25	<1.00	<1.25	<1.50	<1.70	<1.70
	Background	11	<1.50	<1.50	<1.70	<1.70	<1.70
Chromium (µg/L)	Slag-contact	21	<2.00	<5.10	<5.10	<5.80	9.20
	Slag-affected	25	<1.00	4.55	<5.10	<5.80	<5.80
	Background	11	<5.10	<5.10	< 5.80	<5.80	<5.80
Cobalt (µg/L)	Slag-contact	21	<2.00	<2.50	<2.50	<3.70	19.7
	Slag-affected	25	<1.00	1.75	<2.50	<3.70	6.10
	Background	11	<2.50	<2.50	<3.70	<3.70	<3.70
Copper (µg/L)	Slag-contact	21	<2.00	<4.00	<4.00	<4.20	1,660
	Slag-affected	25	<1.00	3.50	<4.20	<4.20	11.5
	Background	11	<4.00	<4.00	<4.20	<4.20	7.50
Iron (µg/L)	Slag-contact	21	12.0	37.0	160	1,190	58,400
	Slag-affected	25	18.0	214	1,430	3,690	52,200
	Background	11	24.0	72.0	1,980	5,260	29,600

Table 6. Statistical summary of ground-water-quality data from Bairstow Landfill and from the Grand Calumet aquifer,

 Hammond, Ind.—Continued

 Table 6. Statistical summary of ground-water-quality data from Bairstow Landfill and from the Grand Calumet aquifer,

 Hammond, Ind.—Continued

Water-quality property	Well type	Number of samples	Minimum value	1st quartile	Median	3rd quartile	Maximum value
Lead (µg/L)	Slag-contact	21	<1.10	<1.10	1.90	2.10	10.8
	Slag-affected	25	<1.00	<1.10	<1.10	2.30	15.0
	Background	11	<1.10	<1.10	1.60	3.20	4.60
Manganese (µg/L)	Slag-contact	21	<2.00	<2.00	44.0	309	2,460
	Slag-affected	25	<1.80	19.8	99.0	473	1,540
	Background	11	<2.00	82.0	197	383	1,230
Mercury (µg/L)	Slag-contact	18	<.10	<.10	.17	.32	1.1
	Slag-affected	19	<.10	<.10	.11	.15	.18
	Background	11	<.10	<.10	.11	.14	.16
Nickel (µg/L)	Slag-contact	21	<4.70	<4.70	<6.10	11.0	148
	Slag-affected	25	2.00	<4.70	< 6.10	<6.10	38.0
	Background	11	<4.70	<4.70	< 6.10	<6.10	27.5
Selenium (µg/L)	Slag-contact	21	<2.00	<2.30	3.00	3.85	14.3
	Slag-affected	25	<1.00	2.15	<2.30	<2.30	17.2
	Background	11	<2.30	<2.30	<2.30	2.90	3.70
Silver (µg/L)	Slag-contact	21	<2.00	<3.80	< 5.00	< 5.00	5.00
	Slag-affected	25	<1.00	2.40	<3.80	< 5.00	5.00
	Background	11	<3.80	<3.80	<3.80	< 5.00	5.00
Water-quality property	Well type	Number of samples	Minimum value	1st quartile	Median	3rd quartile	Maximum value
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Thallium (µg/L)	Slag-contact	16	<1.10	<1.10	1.85	3.60	7.00
	Slag-affected	19	<1.10	1.30	1.90	2.30	2.80
	Background	10	<1.10	1.35	1.75	2.92	3.80
Vanadium (µg/L)	Slag-contact	18	<2.60	<2.60	3.35	8.15	52.7
	Slag-affected	19	<2.60	<2.60	<3.30	<3.30	9.10
	Background	11	<2.60	<2.60	<3.30	<3.30	5.00
Zinc (µg/L)	Slag-contact	21	2.00	<3.40	<3.70	4.40	531
	Slag-affected	25	3.00	<3.40	<3.70	5.70	28.0
	Background	11	<3.40	<3.70	4.10	411	1,090
Dissolved solids (mg/L)	Slag-contact	18	270	401	742	1,890	5,030
	Slag-affected	26	172	372	624	1,060	2,150
	Background	11	95.0	158	262	622	5,080
Suspended solids (mg/L)	Slag-contact	17	3.00	29.0	54.0	231	5,310
	Slag-affected	20	3.00	4.10	14.0	43.1	214
	Background	11	3.00	3.00	3.00	8.50	15.5
Total organic carbon (mg/L)	Slag-contact	17	3.7	6.80	15.1	48.5	209
	Slag-affected	20	2.00	4.17	5.60	13.4	24.7
	Background	11	2.00	2.90	4.80	11.6	26.9
Cyanide (µg/L)	Slag-contact	18	<10.0	<10.0	<10.0	16.6	212
	Slag-affected	19	<10.0	<10.0	<10.0	<10.0	31.4
	Background	11	<10.0	<10.0	<10.0	<10.0	<10.0

Table 6. Statistical summary of ground-water-quality data from Bairstow Landfill and from the Grand Calumet aquifer,

 Hammond, Ind.—Continued